

Lomond View Designs, LLC

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Ogden, UT 84414

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Structural Calculations

for

Ogden City

(Detached Garage)

for

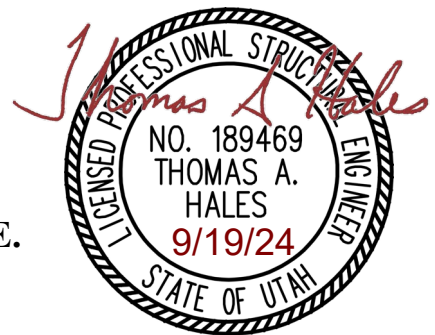
874 E Cahoon Circle

Ogden, Utah

September 19, 2024

Note: These calculations are to be used only for the plan number and the building lot and/or address shown above. Use of these calculations for any other plan or location is prohibited unless written/signed agreement is obtained from Thomas A. Hales indicating otherwise.

Prepared By:
Thomas A. Hales, Ph.D., S.E.



Job # 24025 (Repeat #23098)

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DESIGN CRITERIA:

A. GOVERNING BUILDING CODE: 2021 INTERNATIONAL BUILDING CODE (IBC) AND 2021 INTERNATIONAL RESIDENTIAL CODE (IRC)

B. GRAVITY LIVE LOADING:

1. ROOF: 30 PSF SNOW LOAD
2. FLOOR: 40 PSF LIVE LOAD
3. DECK: 60 PSF LIVE LOAD

C. EARTHQUAKE: $V = S_{ds} * I * W / R = 2/3 * S_{ms} * I * W / R$

1. S_{ms} = USE 1.6 (SDC = 'D2')
2. I, IMPORTANCE FACTOR = 1.0
3. R, BUILDING TYPE = 6.5 (USE 6)
4. W, WEIGHT OF STRUCTURE

D. WIND:

1. VELOCITY: 115 MPH (LRF) * 0.775 → 90 MPH (ASD), BASIC WIND SPEED (IBC 1609.3.1)
2. EXPOSURE: TYPE C
3. IMP. FACTOR: 1.0, STANDARD OCCUPANCY

E. SOIL BEARING PRESSURE: 1500 PSF ASSUMED BY OWNER

F: SEE DRAWINGS FOR GENERAL NOTES AND CONSTRUCTION REQUIREMENTS

COLUMN AND FOOTING LOADS AND SIZES

Project: **JOB #23098**
 Allow. Soil Bearing Press. **1500 psf**

Date: 11/14/2023
 Engineer: Tom Hales

CONTINUOUS FOOTINGS

Footings/Column Location: **TYP. EXTERIOR WALL**

Alt. Soil Bearing Pressure

COMMENT	TRIBUTARY AREA		WEIGHT	SUB TOTAL	CUM. TOT.
	LENGTH 1	PER 1 FT.			
ROOF SNOW LOAD	13.0 ft		30 psf	390 plf	390 plf
ROOF DEAD LOAD	13.0 ft		17 psf	221 plf	611 plf

TOTAL LOAD	611 plf
REQ'D FTG. WIDTH	0.4 ft

USE FC1.7

Footings/Column Location:

Alt. Soil Bearing Pressure

COMMENT	TRIBUTARY AREA		WEIGHT	SUB TOTAL	CUM. TOT.
	LENGTH 1	PER 1 FT.			

TOTAL LOAD	0 plf
REQ'D FTG. WIDTH	0.0 ft

Footings/Column Location:

Alt. Soil Bearing Pressure

COMMENT	TRIBUTARY AREA		WEIGHT	SUB TOTAL	CUM. TOT.
	LENGTH 1	PER 1 FT.			

TOTAL LOAD	0 plf
REQ'D FTG. WIDTH	0.0 ft

WOOD BEAM DESIGN FOR UNIFORM LOADING CONDITIONS

Project: JOB #23098
Description: 16'-0" GARAGE DOOR HEADER

Date: 11/14/2023
Engineer: TAH

INPUT:

Length of Span - L (ft): 17
Distance from Support to Calc. Shear - d (in): 7

Roof Loads:

Trib. Length (ft): 6
Snow Load (psf): 30
Dead Load (psf): 17

Linear Loads:

Snow Load (plf): 0
Live Load (plf): 0
Dead Load (plf): 0

Floor Loads:

Trib. Length (ft): 0
Live Load (psf): 40
Dead Load (psf): 15

Total Load Deflection Criteria (Span/ Δ) - Δ : 240
Live Load Deflection Criteria (Span/ Δ) - Δ : 360

Total Load (plf): 282 plf
Total Live Load (plf): 180 plf

Beam	DL=	867 lbs
Reactions:	LL=	1530 lbs
	TL=	2397 lbs

OUTPUT:

DOUGLAS FIR-LARCH

Allowable Shear Stress - Fv (psi): 95
Modulus of Elasticity - E (ksi): 1600
Allowable Bending Stress - Fb (psi): 1313 2x4
1139 2x6
1052 2x8
961 2x10
845 2x12

I (TL) (in⁴): 389.66
I (LL) (in⁴): 373.08
A (in²): 35.25
S (in³) 2x4: 93.11
2x6: 107.33
2x8: 116.20
2x10: 127.21
2x12: 144.67

GLUED-LAMINATED (24F-V4)

Allowable Shear Stress - Fv (psi): 190
Modulus of Elasticity - E (ksi): 1800
Allowable Bending Stress - Fb (psi): 2400

I (TL) (in⁴): 346.37
I (LL) (in⁴): 331.63
A (in²): 17.63
S (in³): 50.94

3.125 x 12 GLB (0.77)
5.125 x 10.5 GLB (0.7)

MICRO-LAM

Allowable Shear Stress - Fv (psi): 285
Modulus of Elasticity - E (ksi): 1900
Allowable Bending Stress - Fb (psi): 2600

EI (TL) k-in²): 623460
EI (LL) (k-in²): 596930
Shear (lbs): 2233
Moment (ft-lb): 10187

(2)-1.75 x 11.875 M-L (0.67)
(3)-1.75 x 9.5 M-L (0.88)

VERSA-LAM

Allowable Shear Stress - Fv (psi): 285
Modulus of Elasticity - E (ksi): 2000
Allowable Bending Stress - Fb (psi): 2800

EI (TL) k-in²): 623460
EI (LL) (k-in²): 596930
Shear (lbs): 2233
Moment (ft-lb): 10187

(2)-1.75 x 11.25 V-L (0.75)
(3)-1.75 x 9.25 V-L (0.9)

NOTE: A LOAD DURATION FACTOR OF 1.0 IS USED FOR ALL BEAMS

IBC LATERAL ANALYSIS

Project: JOB #23098
Description: MAIN LATERAL

Date: 11/14/2023
Engineer: Tom Hales

Seismic ($V=2/3 \cdot S_{ms} \cdot I \cdot W/R \cdot (1/1.4)$)

$I = 1$
 $S_{ms} = F_a \cdot S_s = 1.6$ NOTE: Site Class D is assumed
 $R = 6$
 $2/3 \cdot S_{ms} \cdot I / R / 1.4 = 0.1270$ (ASD)

Wind 90 mph Basic Wind Speed

	p_{s30}	p_s
Exposure = C	A = 14.4 psf	17.4 psf
Exp Coef = 1.21	B = 9.9 psf	12.0 psf
$K_{zt} = 1$	C = 11.5 psf	13.9 psf
$I_w = 1$	D = 7.9 psf	9.6 psf

roof height = 8.0 ft (top of wall to ridge)

Building Info.

Wall Weight = 12 psf
 Roof Weight = 17 psf
 Seismic snow =
 Total Roof Weight = 17 psf
 Floor to Roof Height = 9 ft
 Building Width = 22 ft
 Building Length = 22 ft
 Building Height = 17 ft
 a = 3.0 ft

Veneer

	Weights (pounds)	Veneer	Total Weights (pounds)	
Wall	1188	0	10604	Dir. perp. to width
Wall	1188	0	10604	Dir. perp. to length
Roof	8228		12980	Tot. Building Wt.
		Vmid =	1648.3	

Seismic Shear Forces

Diaphragm Shears: (per side)	pounds	plf
Walls perpendicular to building width:	673	31
Walls perpendicular to building length:	673	31

Mid-Ht Wall Shears: (per side)	pounds	plf
Walls perpendicular to building width:	824	37
Walls perpendicular to building length:	824	37

USE 7/16" SHEATHING w/8d NAILS @ 6" o.c. G.F. 170plf

SHEARWALLS

350 plf
req'd length
1.9 ft
1.9 ft

Wind Shear Forces

Diaphragm Shears: (per side)	pounds	plf
Walls perpendicular to building width:	1712	78
Walls perpendicular to building length:	1712	78

Mid-Ht Wall Shears: (per side)	pounds	plf
Walls perpendicular to building width:	1712	78
Walls perpendicular to building length:	1712	78

USE 7/16" SHEATHING w/8d NAILS @ 6" o.c. G.F. 240plf

SHEARWALLS

490 plf
req'd length
3.5 ft
3.5 ft

Note: Veneer is assumed to resist it's own in-plane shear.

SHEAR & OVERTURNING ANALYSIS

Project: JOB #23098
Description: MAIN LATERAL

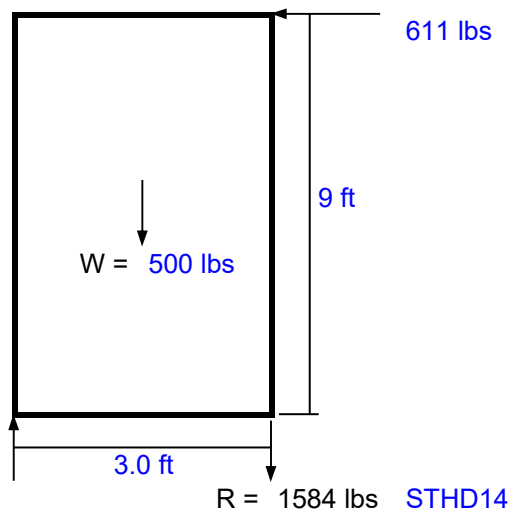
Date: 11/14/2023
Engineer: Tom Hales

SHEAR WALL CHECK

Shear Wall Capacity: 350 plf 4"O.C. EDGE NAILING
Total Shear: 1223 lbs
Req'd Wall Length: 3 ft PLENTY OF WALL AVAILABLE

WALL OVERTURNING

Description: TYP. 3'-0" FRONT WALL PIECES



WALL OVERTURNING

Description: 15'-0" SIDE WALL PIECE

