

**Lomond View Designs, LLC**

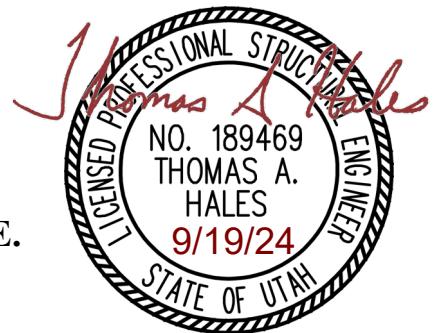
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**Structural Calculations  
for  
Ogden City  
(Detached Garage)  
for  
874 E Cahoon Circle  
Ogden, Utah**

September 19, 2024

Note: These calculations are to be used only for the plan number and the building lot and/or address shown above. Use of these calculations for any other plan or location is prohibited unless written/signed agreement is obtained from Thomas A. Hales indicating otherwise.

Prepared By:  
**Thomas A. Hales, Ph.D., S.E.**



Job # 24025 (Repeat #23098)

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## **DESIGN CRITERIA:**

- A. GOVERNING BUILDING CODE: 2021 INTERNATIONAL BUILDING CODE (IBC) AND 2021 INTERNATIONAL RESIDENTIAL CODE (IRC)
- B. GRAVITY LIVE LOADING:
  - 1. ROOF: 30 PSF SNOW LOAD
  - 2. FLOOR: 40 PSF LIVE LOAD
  - 3. DECK: 60 PSF LIVE LOAD
- C. EARTHQUAKE:  $V = S_{ds} * I * W/R = 2/3 * S_{ms} * I * W/R$ 
  - 1.  $S_{ms} = \text{USE 1.6}$  (SDC = 'D2')
  - 2.  $I$ , IMPORTANCE FACTOR = 1.0
  - 3.  $R$ , BUILDING TYPE = 6.5 (USE 6)
  - 4.  $W$ , WEIGHT OF STRUCTURE
- D. WIND:
  - 1. VELOCITY: 115 MPH (LRF) \* 0.775 → 90 MPH (ASD), BASIC WIND SPEED (IBC 1609.3.1)
  - 2. EXPOSURE: TYPE C
  - 3. IMP. FACTOR: 1.0, STANDARD OCCUPANCY
- E. SOIL BEARING PRESSURE: 1500 PSF ASSUMED BY OWNER
- F: SEE DRAWINGS FOR GENERAL NOTES AND CONSTRUCTION REQUIREMENTS

# COLUMN AND FOOTING LOADS AND SIZES

Project: JOB #23098

Date: 11/14/2023

Allow. Soil Bearing Press. 1500 psf

Engineer: Tom Hales

## CONTINUOUS FOOTINGS

Footing/Column Location: TYP. EXTERIOR WALL

Alt. Soil Bearing Pressure

COMMENT	TRIBUTARY AREA			SUB TOTAL	CUM. TOT.
	LENGTH 1	PER 1 FT.	WEIGHT		
ROOF SNOW LOAD	13.0 ft		30 psf	390 plf	390 plf
ROOF DEAD LOAD	13.0 ft		17 psf	221 plf	611 plf

TOTAL LOAD 611 plf  
REQ'D FTG. WIDTH 0.4 ft USE FC1.7

Footing/Column Location:

Alt. Soil Bearing Pressure

COMMENT	TRIBUTARY AREA			SUB TOTAL	CUM. TOT.
	LENGTH 1	PER 1 FT.	WEIGHT		

TOTAL LOAD 0 plf  
REQ'D FTG. WIDTH 0.0 ft

Footing/Column Location:

Alt. Soil Bearing Pressure

COMMENT	TRIBUTARY AREA			SUB TOTAL	CUM. TOT.
	LENGTH 1	PER 1 FT.	WEIGHT		

TOTAL LOAD 0 plf  
REQ'D FTG. WIDTH 0.0 ft

**WOOD BEAM DESIGN  
FOR UNIFORM LOADING CONDITIONS**

**Project:** JOB #23098  
**Description:** 16'-0" GARAGE DOOR HEADER

**Date:** 11/14/2023  
**Engineer:** TAH

**INPUT:**

Length of Span - L (ft): **17**  
Distance from Support to Calc. Shear - d (in) **7**

**Roof Loads:**

Trib. Length (ft): **6**  
Snow Load (psf): **30**  
Dead Load (psf): **17**

**Floor Loads:**

Trib. Length (ft): **0**  
Live Load (psf): **40**  
Dead Load (psf): **15**

**Linear Loads:**

Snow Load (plf): **0**  
Live Load (plf): **0**  
Dead Load (plf): **0**

Total Load Deflection Criteria (Span/Δ) - Δ: **240**  
Live Load Deflection Criteria (Span/Δ) - Δ: **360**

Total Load (plf): **282 plf**

Total Live Load (plf): **180 plf**

Beam	DL=	<b>867 lbs</b>
Reactions:	LL=	<b>1530 lbs</b>
	TL=	<b>2397 lbs</b>

**OUTPUT:**

**DOUGLAS FIR-LARCH**

Allowable Shear Stress - Fv (psi):	<b>95</b>	I (TL) (in^4): <b>389.66</b>
Modulus of Elasticity - E (ksi):	<b>1600</b>	I (LL) (in^4): <b>373.08</b>
Allowable Bending Stress - Fb (psi):	<b>1313 2x4</b>	A (in^2): <b>35.25</b>
	<b>1139 2x6</b>	S (in^3) 2x4: <b>93.11</b>
	<b>1052 2x8</b>	2x6: <b>107.33</b>
	<b>961 2x10</b>	2x8: <b>116.20</b>
	<b>845 2x12</b>	2x10: <b>127.21</b>
		2x12: <b>144.67</b>

**GLUED-LAMINATED (24F-V4)**

Allowable Shear Stress - Fv (psi):	<b>190</b>	I (TL) (in^4): <b>346.37</b>
Modulus of Elasticity - E (ksi):	<b>1800</b>	I (LL) (in^4): <b>331.63</b>
Allowable Bending Stress - Fb (psi):	<b>2400</b>	<b>3.125 x 12 GLB (0.77)</b>
		<b>5.125 x 10.5 GLB (0.7)</b>
		A (in^2): <b>17.63</b>
		S (in^3): <b>50.94</b>

**MICRO-LAM**

Allowable Shear Stress - Fv (psi):	<b>285</b>	EI (TL) k-in^2: <b>623460</b>
Modulus of Elasticity - E (ksi):	<b>1900</b>	EI (LL) (k-in^2): <b>596930</b>
Allowable Bending Stress - Fb (psi):	<b>2600</b>	Shear (lbs): <b>2233</b>
		Moment (ft-lb): <b>10187</b>

**3.125 x 12 GLB (0.77)**

**5.125 x 10.5 GLB (0.7)**

**VERSA-LAM**

Allowable Shear Stress - Fv (psi):	<b>285</b>	EI (TL) k-in^2: <b>623460</b>
Modulus of Elasticity - E (ksi):	<b>2000</b>	EI (LL) (k-in^2): <b>596930</b>
Allowable Bending Stress - Fb (psi):	<b>2800</b>	Shear (lbs): <b>2233</b>
		Moment (ft-lb): <b>10187</b>

**(2)-1.75 x 11.875 M-L (0.67)**

**(3)-1.75 x 9.5 M-L (0.88)**

**(2)-1.75 x 11.25 V-L (0.75)**

**(3)-1.75 x 9.25 V-L (0.9)**

NOTE: A LOAD DURATION FACTOR OF 1.0 IS USED FOR ALL BEAMS

## IBC LATERAL ANALYSIS

**Project:** JOB #23098  
**Description:** MAIN LATERAL

**Date:** 11/14/2023  
**Engineer:** Tom Hales

**Seismic (V=2/3\*Sms\*I\*W/R\*(1/1.4))**

I = 1

Sms=Fa\*Ss 1.6      NOTE: Site Class D is assumed

R = 6

2/3\*Sms\*I/R/1.4) = 0.1270      (ASD)

<u>Wind</u>	90 mph	Basic Wind Speed	$p_{s30}$	$p_s$
Exposure =	C	A =	14.4 psf	17.4 psf
Exp Coef =	1.21	B =	9.9 psf	12.0 psf
$K_{zt}$ =	1	C =	11.5 psf	13.9 psf
$I_w$ =	1	D =	7.9 psf	9.6 psf
roof height =	8.0 ft	(top of wall to ridge)		

**Building Info.**

	<u>Veneer</u>			
	Weights (pounds)	Veneer	Total Weights (pounds)	
Wall Weight =	12 psf			
Roof Weight =	17 psf			
Seismic snow =				
Total Roof Weight =	17 psf	Wall 1188	0 10604	Dir. perp. to width
Floor to Roof Height =	9 ft	Wall 1188	0 10604	Dir. perp. to length
Building Width =	22 ft	Roof 8228	12980	Tot. Building Wt.
Building Length =	22 ft		Vmid = 1648.3	
Building Height =	17 ft			
a=	3.0 ft			

**Seismic Shear Forces**

Diaphragm Shears: (per side)	<u>pounds</u>	<u>plf</u>	<u>350 plf</u>
Walls perpendicular to building width:	673	31	req'd length
Walls perpendicular to building length:	673	31	1.9 ft

Mid-Ht Wall Shears: (per side)	<u>pounds</u>	<u>plf</u>	<u>350 plf</u>
Walls perpendicular to building width:	824	37	req'd length
Walls perpendicular to building length:	824	37	1.9 ft

**USE 7/16" SHEATHING w/8d NAILS @ 6" o.c. G.F. 170plf**

**Wind Shear Forces**

Diaphragm Shears: (per side)	<u>pounds</u>	<u>plf</u>	<u>490 plf</u>
Walls perpendicular to building width:	1712	78	CONTROLS=>
Walls perpendicular to building length:	1712	78	CONTROLS=>

Mid-Ht Wall Shears: (per side)	<u>pounds</u>	<u>plf</u>	<u>490 plf</u>
Walls perpendicular to building width:	1712	78	CONTROLS=>
Walls perpendicular to building length:	1712	78	CONTROLS=>

**USE 7/16" SHEATHING w/8d NAILS @ 6" o.c. G.F. 240plf**

Note: Veneer is assumed to resist its own in-plane shear.

## SHEAR & OVERTURNING ANALYSIS

Project: JOB #23098  
Description: MAIN LATERAL

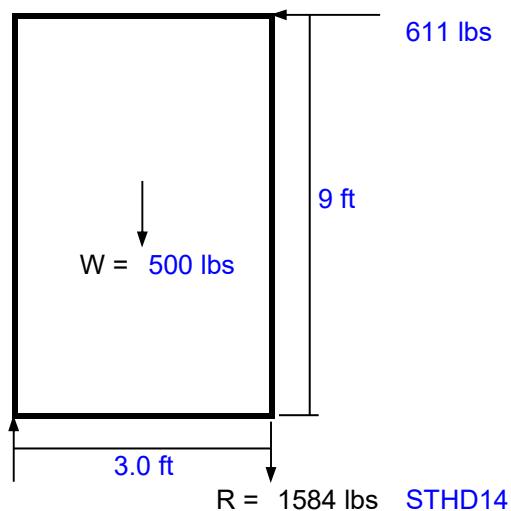
Date: 11/14/2023  
Engineer: Tom Hales

### SHEAR WALL CHECK

Shear Wall Capacity: 350 plf 4"O.C. EDGE NAILING  
Total Shear: 1223 lbs  
Req'd Wall Lngth: 3 ft PLENTY OF WALL AVAILABLE

### WALL OVERTURNING

Description: TYP. 3'-0" FRONT WALL PIECES



### WALL OVERTURNING

Description: 15'-0" SIDE WALL PIECE

